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Managing high voltage line ripple rejection using high bandwidth DC-DC

VICOR

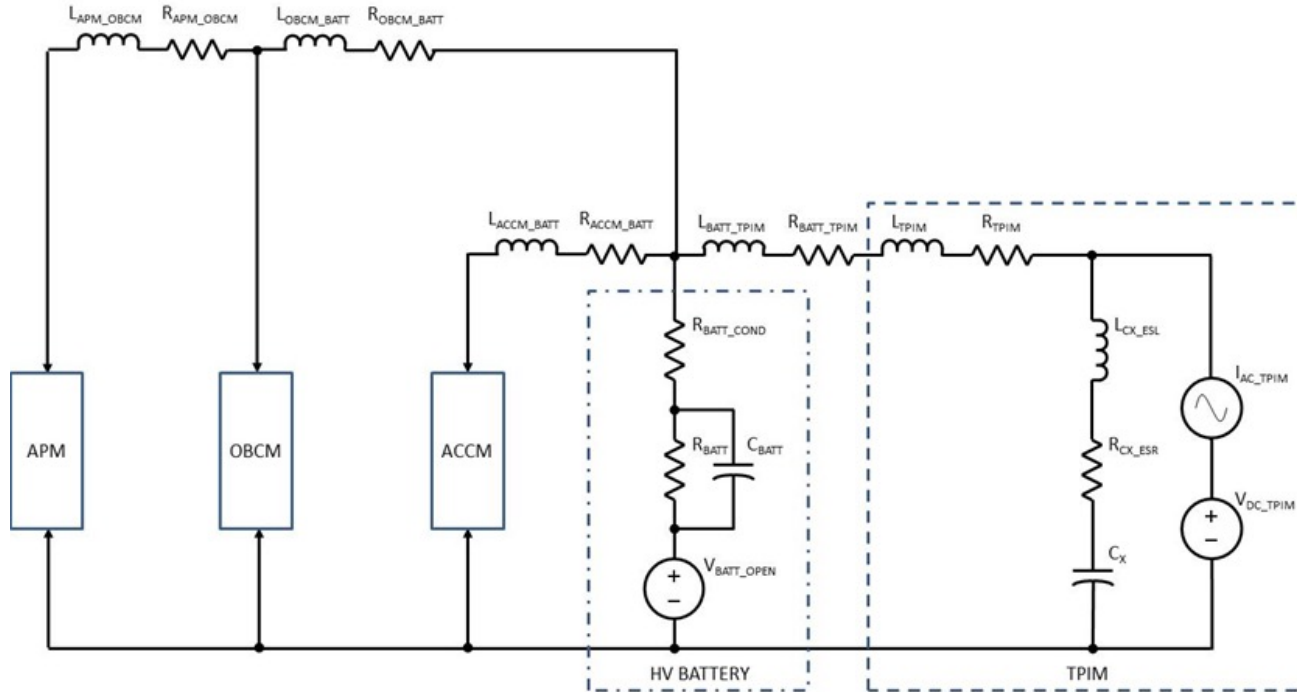
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Electric vehicle HV bus overview and inverter ripple



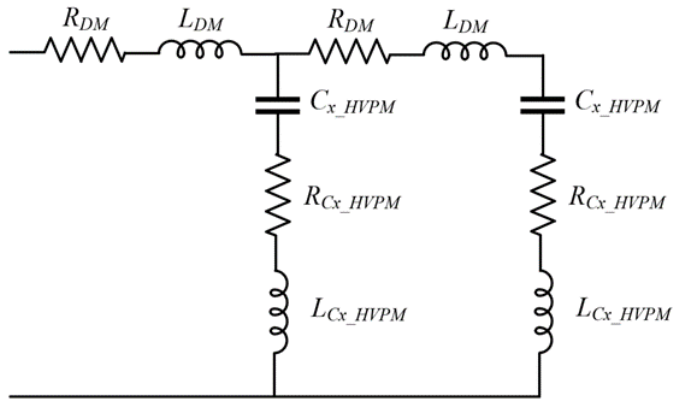
- High voltage ripple occurs on high voltage bus during propulsion and regeneration as a result of inverter's (PIM) operation.
- Most of the ripple is filtered by inverter's bulk capacitor but significant part is injected to HV bus and can cause issues for other power converters.

Impact of inverter ripple on APM (Accessory Power Module)

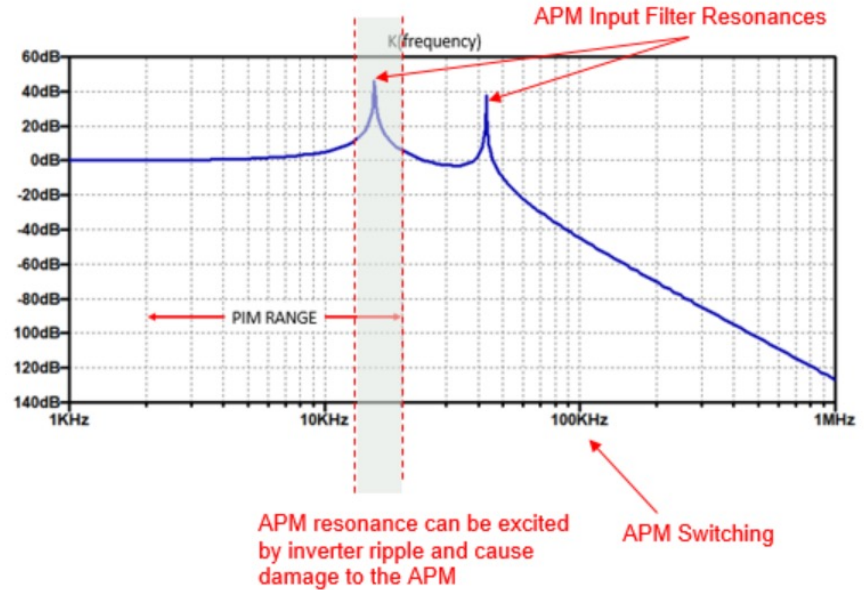
- Component Degradation:
 - APM input filter capacitors are exposed to both APM switching current and inverter ripple
 - Self-heating caused by $(I_{rms}^2 R_{ESR})$ leads to component degradation
- Ripple Transfer to APM Output
 - APM closed-loop bandwidth limited to a few kHz
 - Inverter ripple frequency not rejected by control loop
 - Ripple not filtered by Input filter. Attenuated by transformer
- Audio Noise / Mechanical Resonance
- Component Damage (overvoltage) due to filter gain near resonance
 - Semiconductor devices must block (withstand) both HVDC voltage AND ripple voltage superimposed onto HVDC bus
 - Sufficient Voltage Breakdown Margin required
- Filter resonances excited by inverter ripple will cause damage (over voltage and current)

Resonances: HVPM HVDC filters

- HVDC filters are designed to address EMI noise and not inverter ripple.
- If designed without taking inverter ripple into consideration, the filter can inadvertently be excited by inverter ripple



Circuit Model of a 4-pole APM EMI filter



Ripple rejection - example

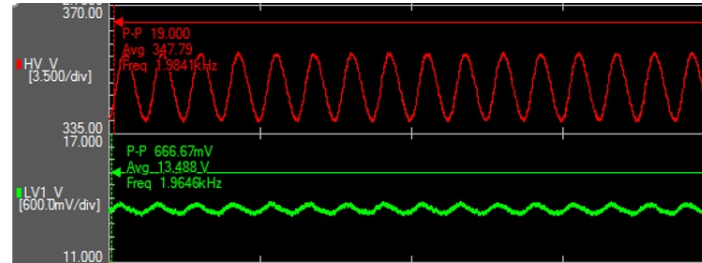
HV Ripple:

Frequency = 2kHz

Magnitude = 19Vp-p

Converter Voltage Ripple

Magnitude: 0.7 Vp-p



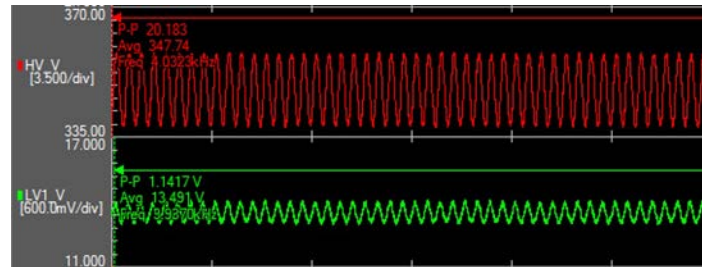
HV Ripple:

Frequency = 4kHz

Magnitude = 20Vp-p

Converter Voltage Ripple

Magnitude: 1.14 Vp-p



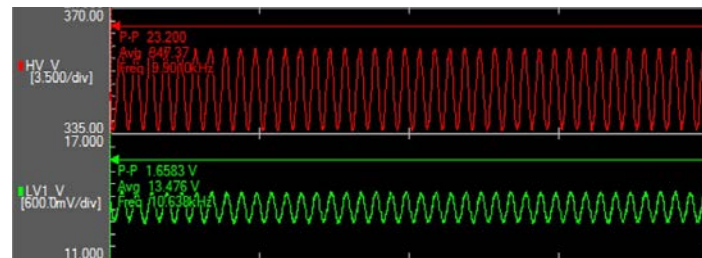
HV Ripple:

Frequency = 10kHz

Magnitude = 23Vp-p

Converter Voltage Ripple

Magnitude: 1.7 Vp-p



Solutions to address inverter ripple

- Minimize Inverter Ripple on HV Bus:
 - Modify Drive Profiles
 - Increase DC Link Capacitance
 - Implement “No-fly” Zones to avoid exciting component resonances
- Design Converters which operate significantly higher above potential oscillations (ripple) on HV bus. The advantages are:
 - DCDC converter at high switching frequency able to reject line ripple
 - Higher resonance for input filter means smaller filter size

High frequency, soft switching DC-DC and impact on EMI filter

- Increased power density
- Minimized voltage and current ripple
- Minimized EMI filtering effort
- Closed loop control bandwidth extended

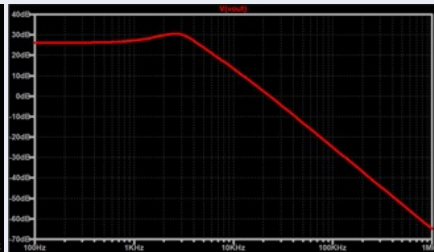
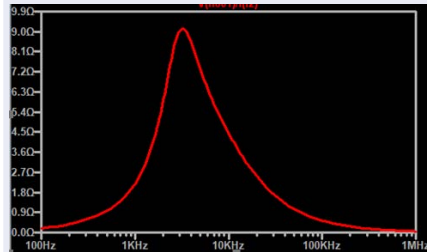
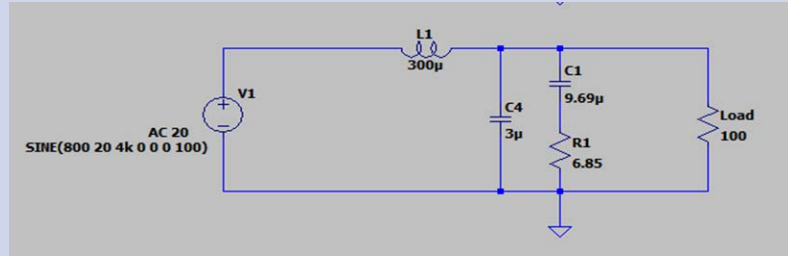
Example/filter design: design steps

1. Select the cut-off frequency below the crossover frequency of the converter
2. Choose the inductor L based on maximum input current, calculate C based on equation or determine C based on voltage level and calculate L
3. Select appropriate filter network and calculate component values based on equations
 - Assume peak output impedance of the filter to be at least 10 times lower than input impedance of converter
 - For 500V input and 2.5kW converter $Z_{in}=100$ Ohm

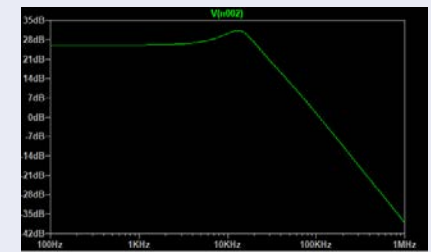
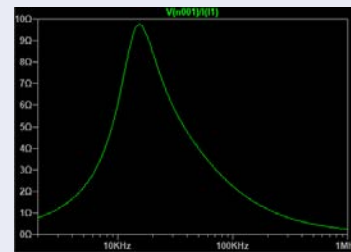
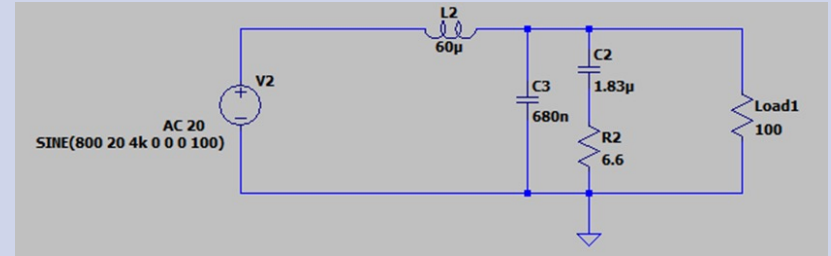
Apply these steps for two different DC-DC converters with 5kHz and 25kHz filter cut-off

Filter comparison

5kHz cut-off

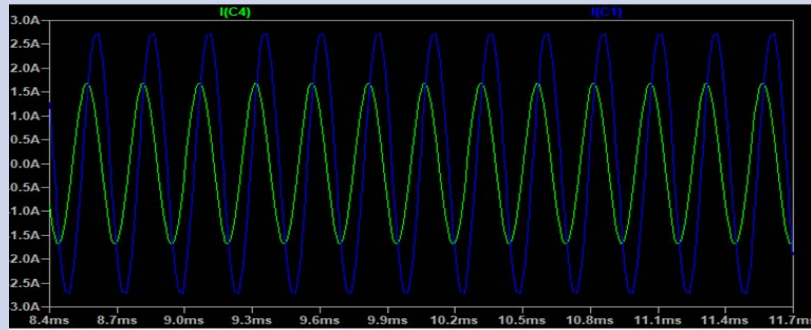


25kHz cut-off



Filter comparison- applying ripple voltage on HV input bus

5kHz cut-off



Waveform: I(C4) ×

Interval Start: 8.4ms

Interval End: 11.7ms

Average: |22.049mA

RMS: 1.1904A

Waveform: I(C1) ×

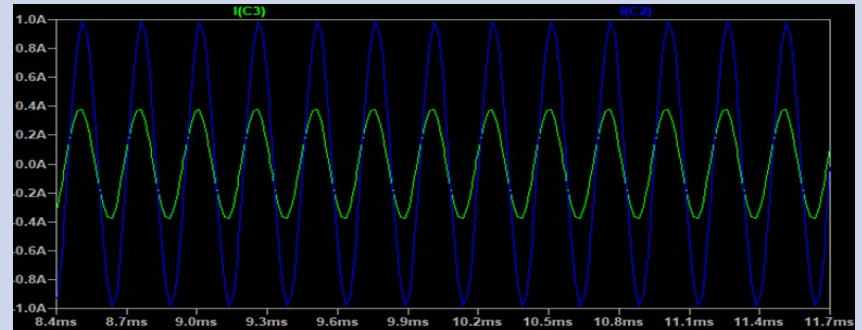
Interval Start: 8.4ms

Interval End: 11.7ms

Average: |5.5372mA

RMS: 1.9315A

25kHz cut-off



Waveform: I(C3) ×

Interval Start: 8.4ms

Interval End: 11.7ms

Average: |1.829mA

RMS: 264.69mA

Waveform: I(C2) ×

Interval Start: 8.4ms

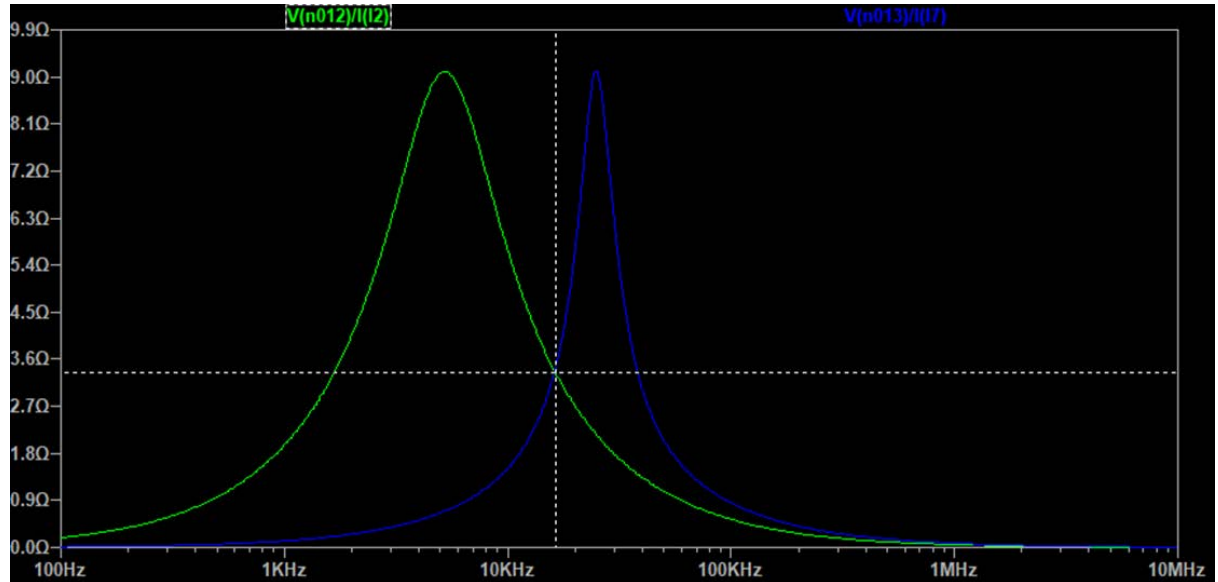
Interval End: 11.7ms

Average: |8.3599mA

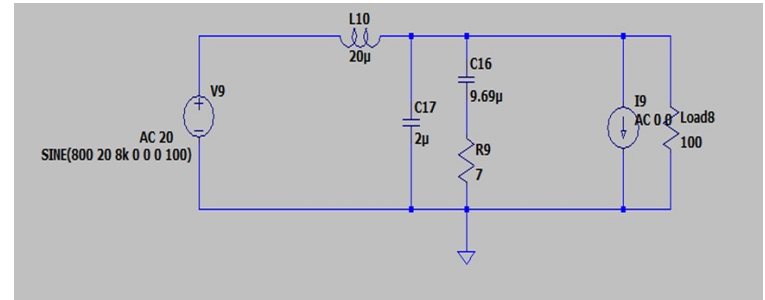
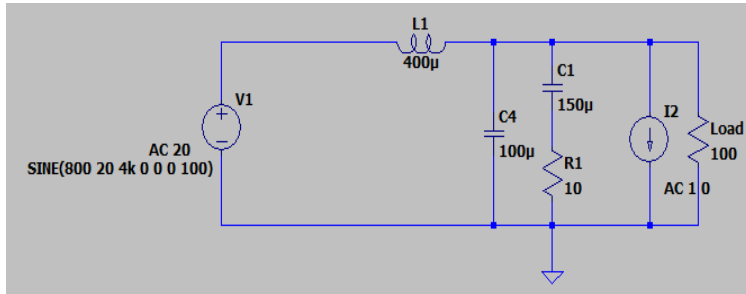
RMS: 683.32mA

Filter output impedance

- In order to keep filter losses lower, output impedance of the high cut-off filter should be below output impedance of the low cut-off, until frequency of interest
- Lower impedance – lower losses, break even point 16kHz



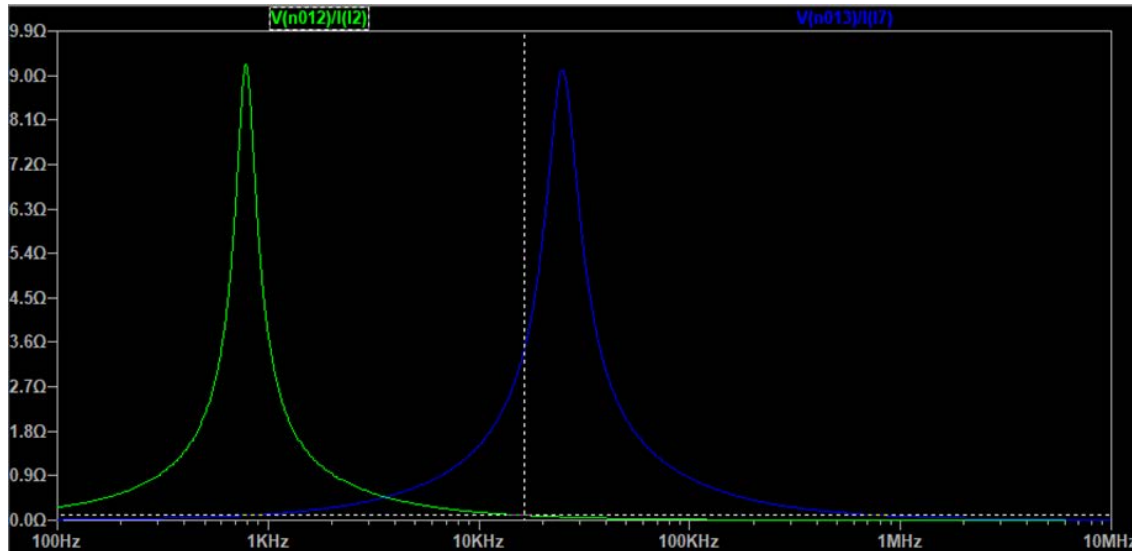
Size comparison - for filters with equal power losses



$L1 = 20 \times L10$
 $C4 = 50 \times C17$

To keep losses equal
and distributed

ONLY EXAMPLE



Filter topology influence

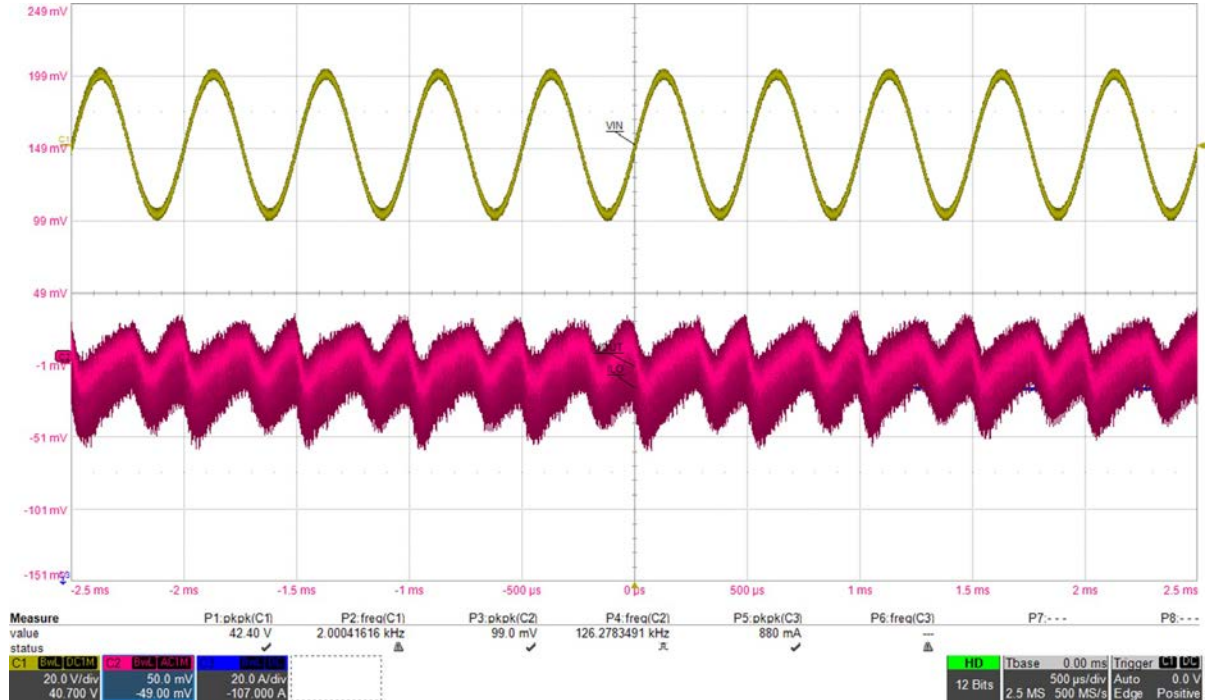
- Undamped filter
 - Risk of uncontrolled voltage amplification
 - Avoid inverter switching frequency
- Simplified damped
 - Weak attenuation at higher frequencies
- Series or parallel damped
 - Dissipate energy in damping circuit
 - Attenuate noise

Series damped might be more attractive due to lower current at high voltage level.

Relative size ratio will remain the same.

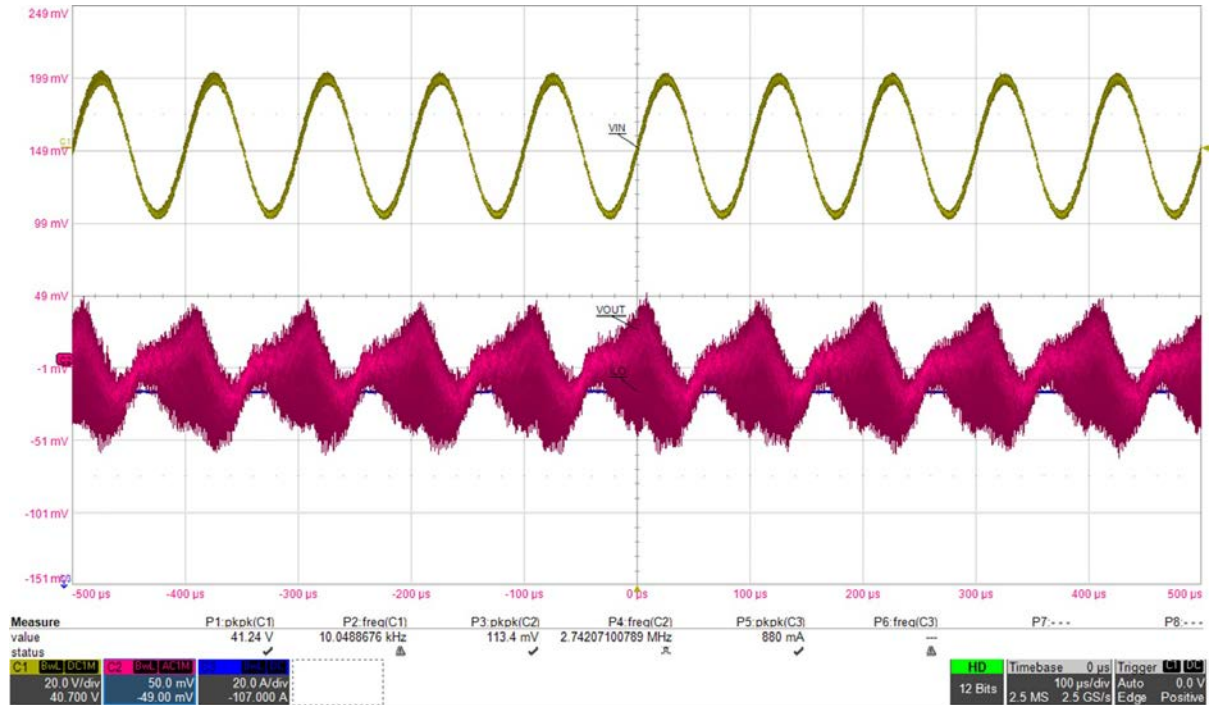
Vicor's DC-DC converter under HV ripple – time domain

$$V_{IN} = 700 + 20 * \sin(2 * \pi * 2k * t)$$



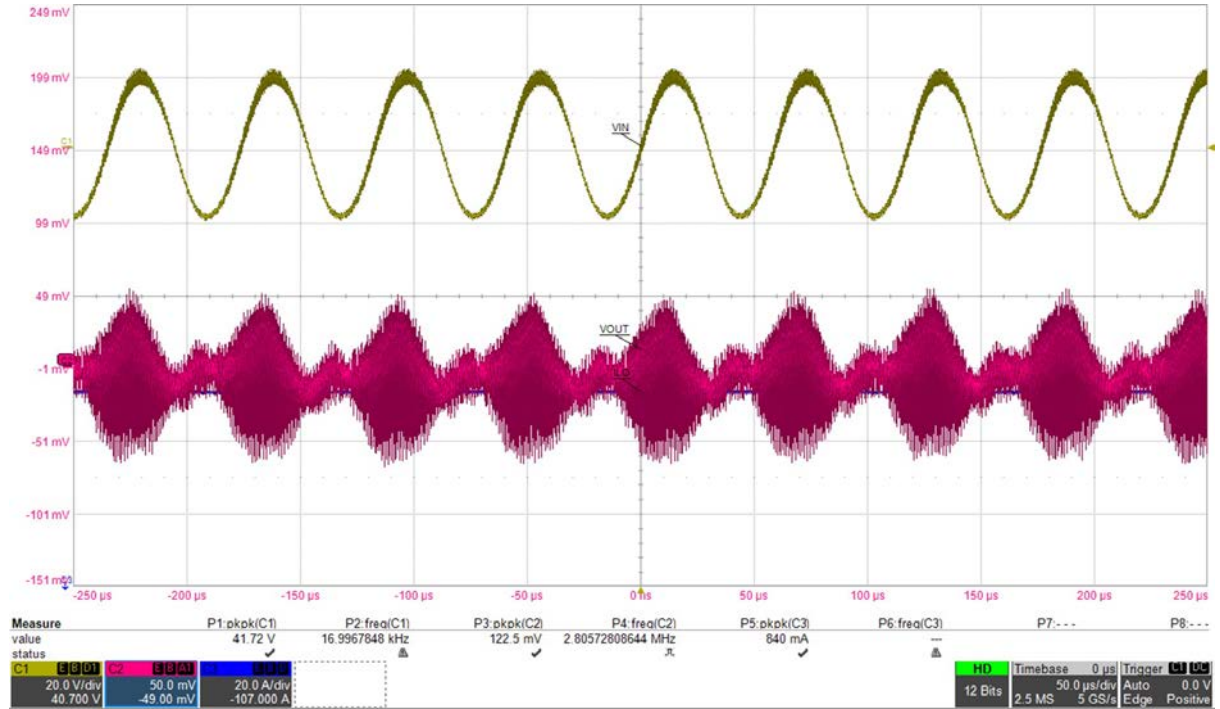
Vicor's DC-DC converter under HV ripple – time domain

$$V_{IN} = 700 + 20 \cdot \sin(2 \cdot \pi \cdot 10k \cdot t)$$

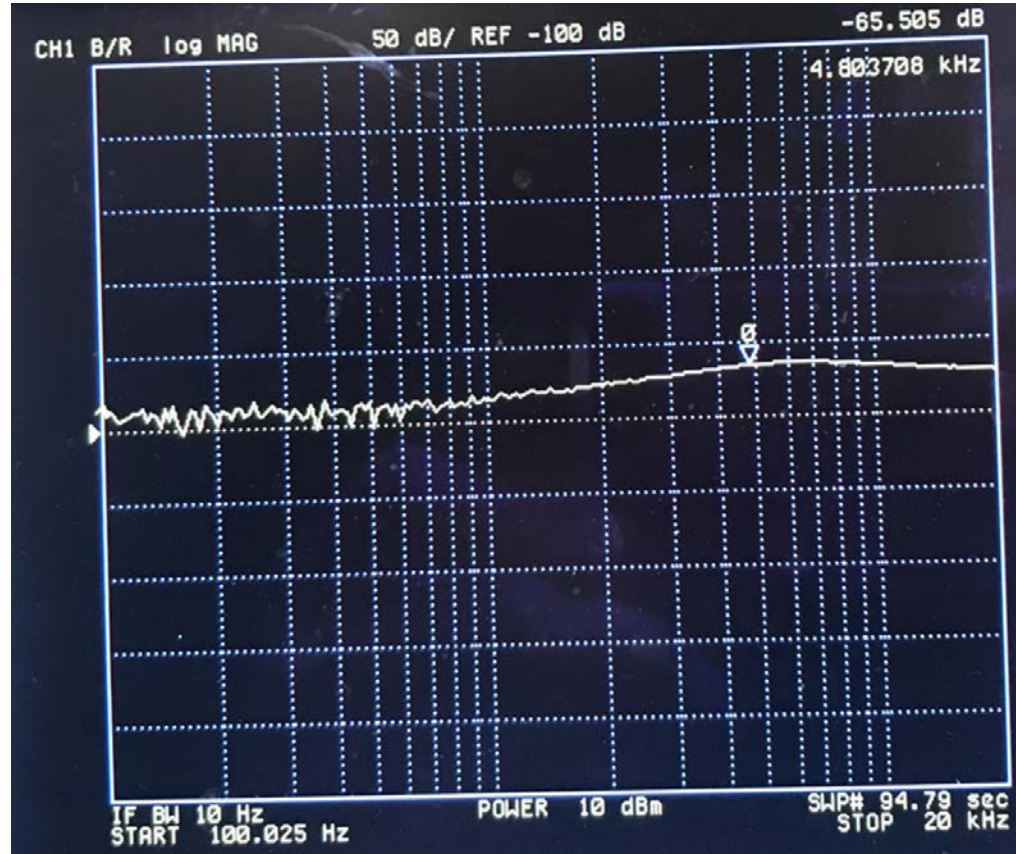


Vicor's DC-DC converter under HV ripple – time domain

$$V_{in} = 700 + 20 \cdot \sin(2 \cdot \pi \cdot 17k \cdot t)$$



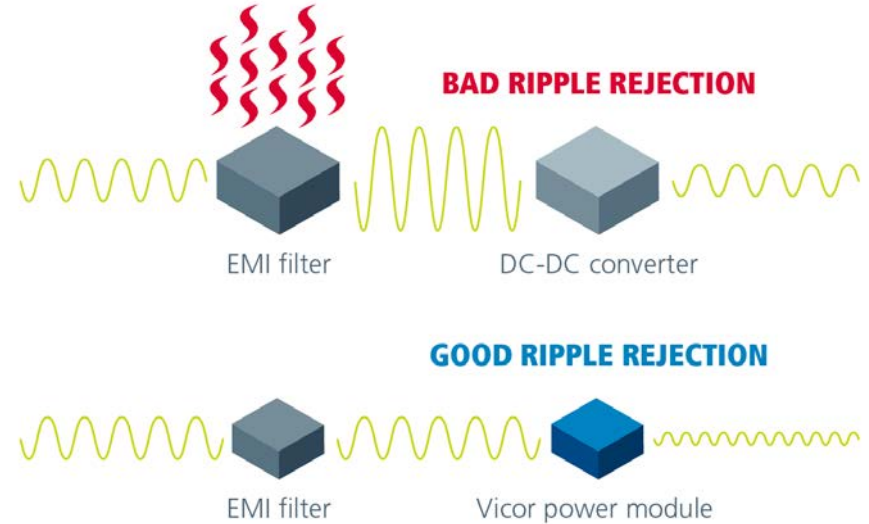
Vicor's DC-DC converter under HV ripple – frequency response



Conclusion

Vicor DC-DC converter enables:

- Highest power density conversion
- Smallest EMI filter (high switching frequency and ZVS/ZCS topology)
 - Shifting frequency range
- Reliable system and simplified architecture
- High frequency enable higher closed loop bandwidth and rejects inverter ripple noise



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